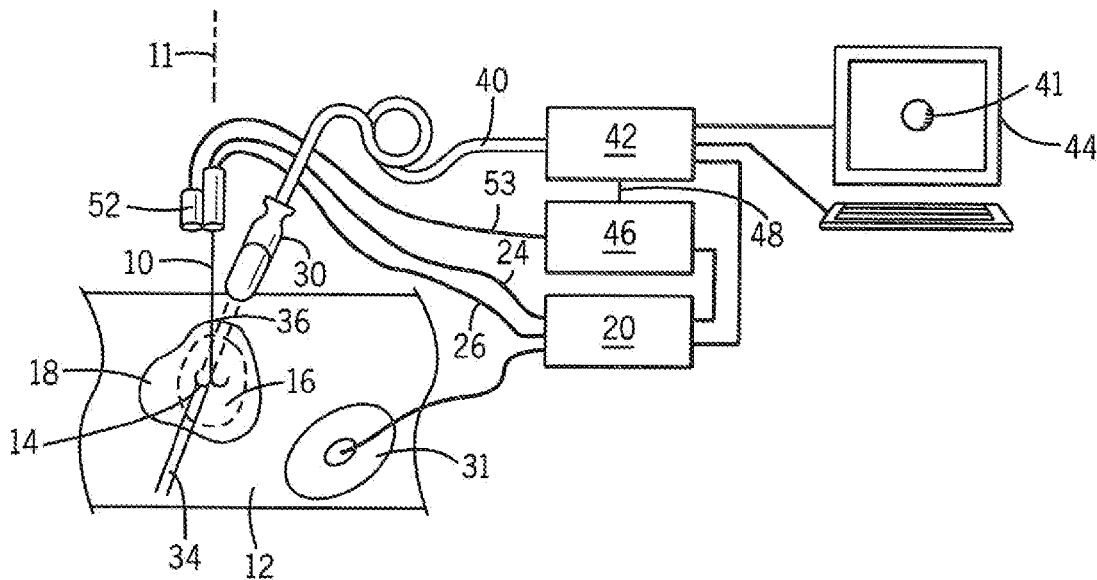




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Varghese et al.(10) **Pub. No.: US 2015/0330832 A1**(43) **Pub. Date: Nov. 19, 2015**(54) **METHOD AND APPARATUS FOR RAPID
ACQUISITION OF ELASTICITY DATA IN
THREE DIMENSIONS****Publication Classification**(51) **Int. Cl.**
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Foundation, Madison, WI (US)**(21) Appl. No.: **14/276,019**(22) Filed: **May 13, 2014**(57) **ABSTRACT**

Interpolation of ultrasound data at regular grid locations is provided by simultaneously optimizing interpolated data according to fidelity of interpolation of the voxel data to actual measured spatial data and according to a gradient of the interpolated data. This process is made amenable to real-time processing by limiting the range of interpolation to produce a sparse interpolated matrix that may be readily inverted. Artifacts and inefficiencies from successive stages of interpolation and data smoothing are thereby avoided.



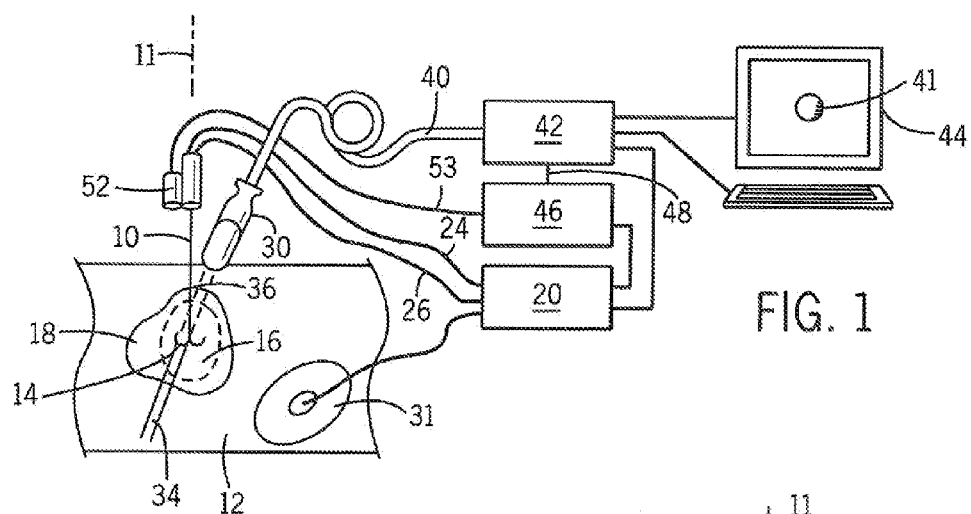


FIG. 1

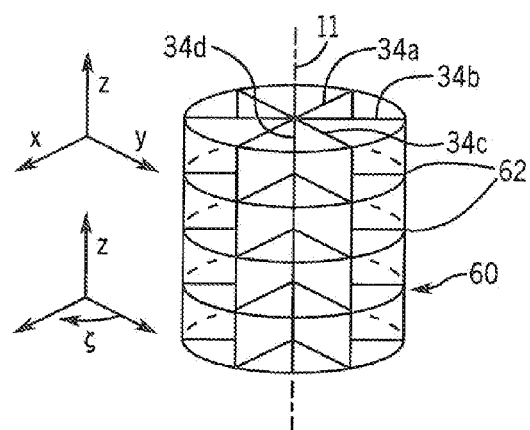


FIG. 2

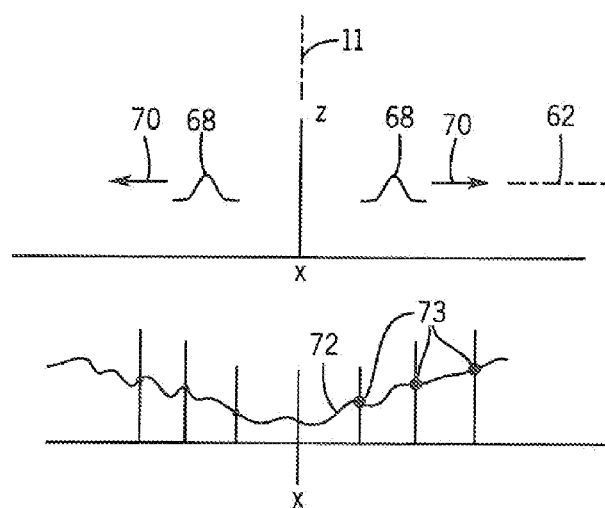


FIG. 3

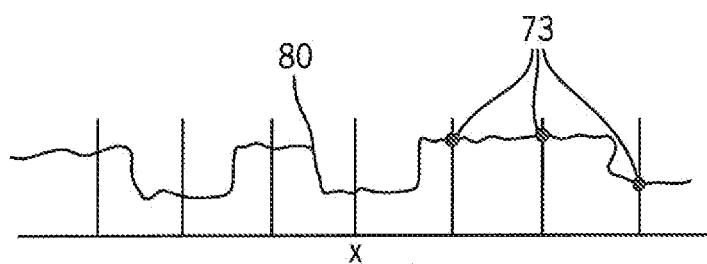


FIG. 4

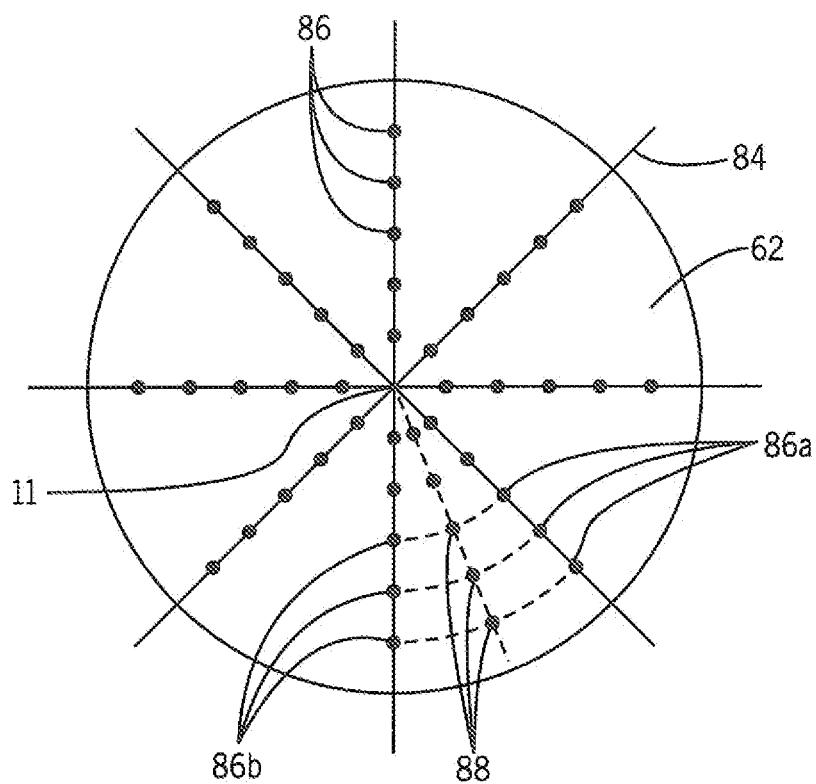
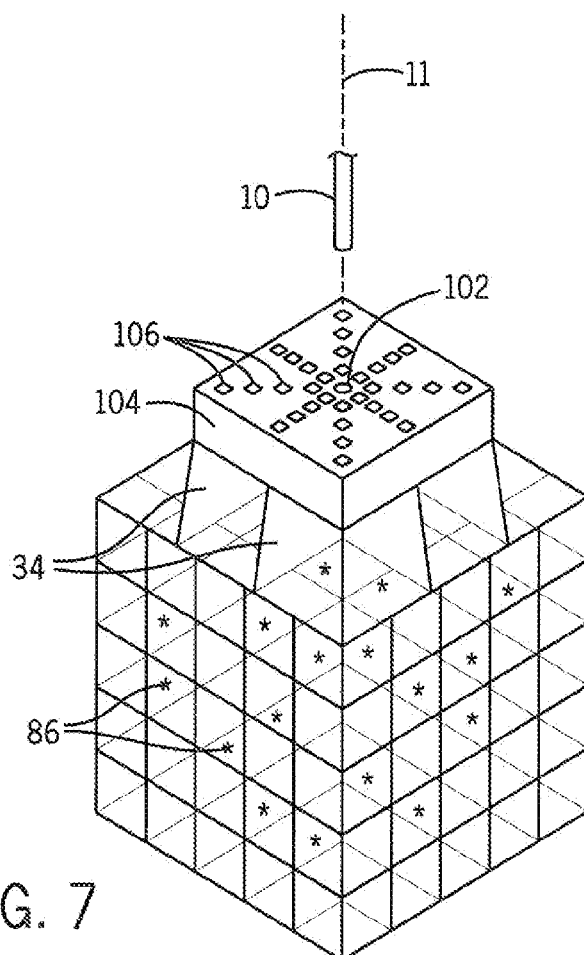
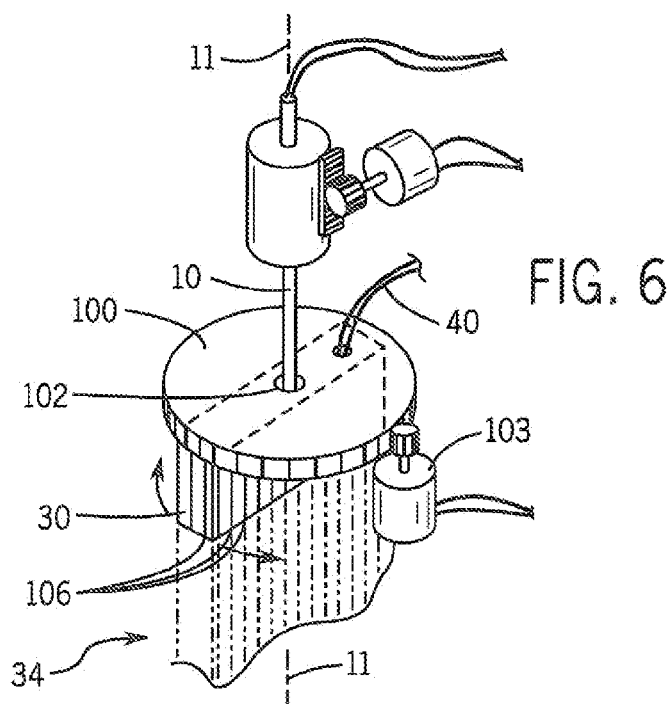


FIG. 5



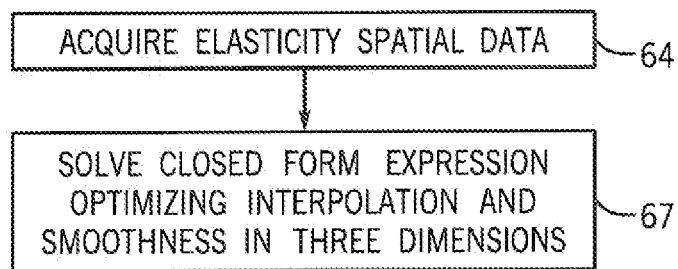


FIG. 8

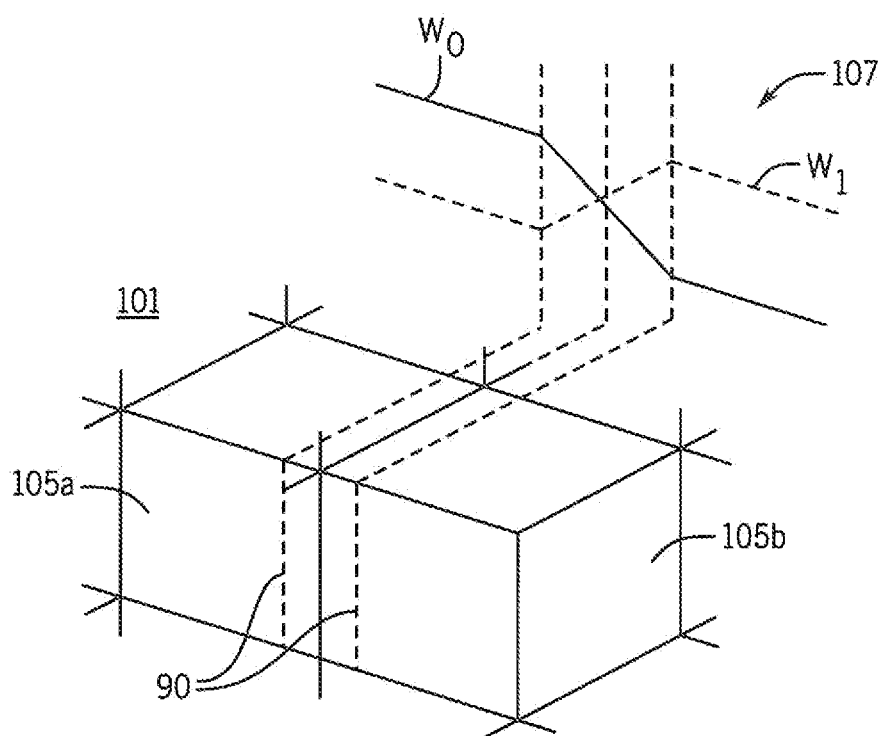


FIG. 9

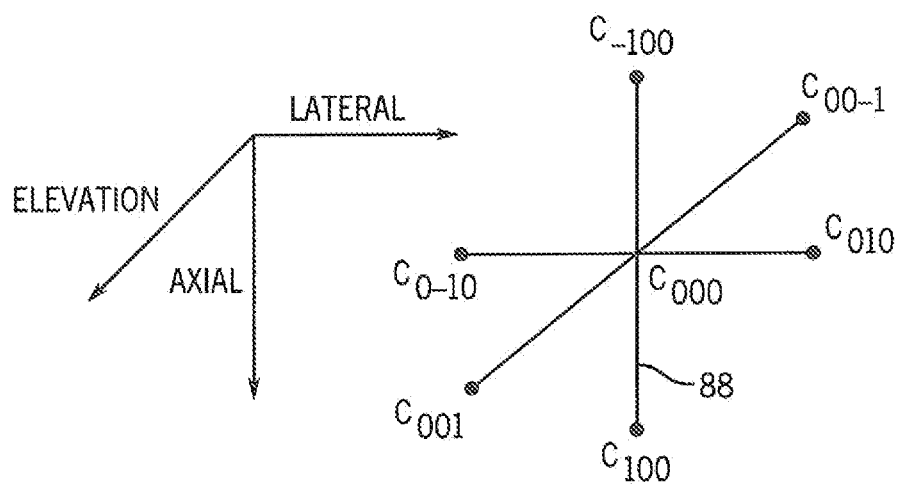


FIG. 10

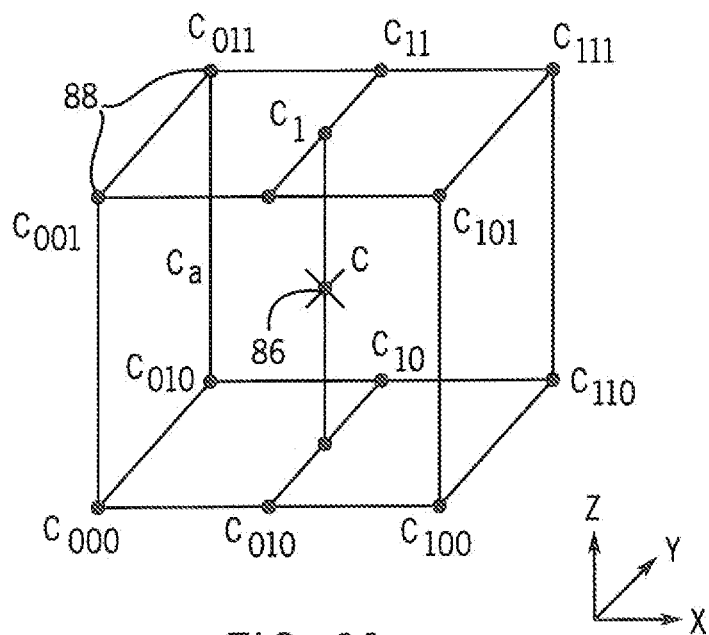


FIG. 11

METHOD AND APPARATUS FOR RAPID ACQUISITION OF ELASTICITY DATA IN THREE DIMENSIONS

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH

[0001] This invention was made with government support under CM 12192 awarded by the National Institutes of Health. The government has certain rights in the invention.

CROSS-REFERENCE TO RELATED APPLICATIONS

[0002] --

BACKGROUND OF THE INVENTION

[0003] The present invention relates to ultrasonic imaging techniques for obtaining information about tissue elasticity and in particular to a method of rapidly acquiring three-dimensional elasticity reconstructions useful, for example, during RF ablation.

[0004] Elastography is an imaging modality that reveals the stiffness properties of tissues, for example, axial strain, lateral strain. Poisson's ratio, shear wave velocity, shear and Young's moduli, or other common stiffness measurements. The stiffness measurements may be output as quantitative values or mapped to a gray or color scale to form a picture over a plane or within a volume.

[0005] Generally, stiffness is deduced by monitoring tissue movement under an applied quasi-static or dynamic force or deformation. The monitoring may be done by any medical imaging modality including computed tomography (CT), magnetic resonance imaging (MRI), and ultrasonic imaging. Elastography of this type is analogous to a physician's palpation of tissue in which the physician determines stiffness by pressing the tissue and detecting the amount that the tissue yields under pressure.

[0006] In "dynamic" elastography, a low frequency vibration is induced in the tissue and the velocity of the resulting compression/shear waves are tracked and measured, for example, using ultrasonic Doppler detection. In "quasi-static" elastography, two images of the tissue are obtained at different states of compression, typically using the ultrasonic transducer as a compression paddle. Displacement of the tissue between the two images is used to deduce the stiffness of the tissue.

[0007] Ideally, elasticity data is acquired over a volume of interest in the tissue, U.S. patent application Ser. No. 13/780,880, filed Feb. 28, 2013, assigned to the same assignee as the present invention and hereby incorporated by reference, describes a system for volumetric ultrasound acquisition which obtains data in a series of radially extending planes positioned at different angles about a common axis.

[0008] With most acquisition patterns, spatial data must be interpolated to regular voxel points along a regular grid so that the data may be displayed through projections as pixels on a display monitor. In the acquisition pattern of radially extending planes described above, data on any of the planes may be first interpolated to regular grid locations within the plane and then interpolation may be conducted between the interpolated data of different planes.

[0009] The spatial data may be relatively noisy and accordingly, within each plane, the spatial data may first be fit to a

model, for example, extracting trends from the data that reduce image artifacts caused by noise.

SUMMARY OF THE INVENTION

[0010] Employing two distinct steps of modeling then interpolating is both time-consuming and may produce a suboptimal fit of the voxel data to the spatial data. Ideally, these processes could be performed simultaneously in three dimensions to better accommodate the trade-off between interpolation fidelity and noise reduction. Generally, global optimization techniques, such as linear programming, can be extremely time-consuming when the number of interpolation grid points is large, and accordingly impractical for generating real-time ultrasound images.

[0011] The present invention addresses these problems by allowing simultaneous three-dimensional interpolation and noise reduction by formulating the problem as a smoothness-constrained trilinear interpolation considering only locally adjacent spatial data points. This problem formulation provides a sparse matrix that may be readily inverted providing a simple closed-form solution that allows the steps of interpolation and noise reduction to be reliably and rapidly executed. Additional time savings can be obtained by separately evaluating subregions of the volume of interest and then joining the subregions together by a simple weighting process.

[0012] Specifically then, in one embodiment, the invention provides apparatus for acquiring three-dimensional ultrasound data including an ultrasonic probe assembly adapted to direct an ultrasound beam into tissue and receive ultrasonic echoes and measure the same to provide ultrasound data, and an electronic computer receiving the ultrasound data and executing a stored program held in non-transitive medium.

[0013] The program executes to process the ultrasound data to obtain spatial data characterizing the tissue at a plurality of discrete locations over three dimensions of a volume of interest within the tissue followed by a determination of the values of voxels in a three-dimensional image grid within the tissue. This determination simultaneously minimizes a combination of an error between each given voxel data and interpolated values of the spatial data selected to be in a region proximate to the voxel data; and a gradient of the voxel data at the given voxel data point location. The region proximate to the voxel data volume is three-dimensional but limited in extent to much less than the dimensions of the entire volume of interest.

[0014] It is a feature of at least one embodiment of the invention to provide improved processing of sparse and noisy ultrasound data in a way that simultaneously accommodates an interpolation and smoothing of the data in three dimensions.

[0015] The interpolation error considered in this process may be a function of a magnitude of a difference between the value of a given element of spatial data and an interpolated value of the surrounding voxels to the location of the spatial data in three dimensions.

[0016] It is thus a feature of at least one embodiment of the invention to provide a simple measure of interpolation fidelity.

[0017] The gradient may be a function of differences among values of adjacent voxel data to the given voxel.

[0018] It is thus a feature of at least one embodiment of the invention to provide an easily calculated measure of smoothness in the image.

[0019] The determination may be performed by selecting a value of each given voxel data to minimize:

$$\|Ac-b\|^2$$

[0020] subject to

$$\|Bc\|^2 \leq M$$

[0021] where: c is the data of the given voxels;

[0022] b is the ultrasonically measured spatial data;

[0023] A is an interpolant matrix performing a linear interpolation of values in c to the locations of data points in b;

[0024] B is a finite differencing gradient matrix representing the gradient in voxel data values at c; and

[0025] M is a constant selected to describe the desired image smoothness.

[0026] It is thus a feature of at least one embodiment of the invention to provide a technique for providing a balancing between interpolation fidelity and smoothness in three dimensions for all voxels.

[0027] The matrix A may be a sparse matrix.

[0028] It is thus a feature of at least one embodiment of the invention to provide a technique well suited to the image processing of sparse ultrasound data which yields a readily invertible matrix.

[0029] The determination may solve the closed form expression:

$$c=(A^T A+\lambda B^T B)^{-1} A^T b$$

where λ is a predetermined value controlling the amount of smoothing of the data.

[0030] It is thus a feature of at least one embodiment of the invention to provide a tractable, closed-form expression for rapidly implementing the present invention.

[0031] The number of points of spatial data within the volume of interest may be less than the number of voxels within the volume of interest.

[0032] It is thus a feature of at least one embodiment of the invention to provide a technique that may work with ill-posed inverse problems that have fewer data points than the number of voxels.

[0033] The region proximate to the data volume may extend only to the closest eight voxels in case of trilinear interpolation. Alternatively or in addition, the voxel data may provide points at regular intervals along three Cartesian dimensions and the region proximate to the voxel data may be a smallest polyhedron that surrounds the spatial data point with voxels at vertex points and wherein the error is calculated only from interpolation at these vertex points.

[0034] It is thus a feature of at least one embodiment of the invention to create a tractable matrix expression by limiting the spatial scope of the interpolation function.

[0035] The interpolated values may be trilinear interpolation in three dimensions.

[0036] It is thus a feature of at least one embodiment of the invention to employ a well-behaved interpolation system that may be spatially limited without undue artifacts.

[0037] The volume of interest may be subdivided into sub-blocks and the above process repeated for multiple sub-blocks and those sub-blocks combined by weighting data at the periphery of adjacent sub-blocks.

[0038] It is thus a feature of at least one embodiment of the invention to permit the optimization process to be performed in available high-speed computer memory (without, for example, disk drive accesses) for high speed commensurate with the need for real time data display.

[0039] The spatial data characterizing the tissue may be a speed of a shear wave through the tissue at the points of spatial data or a function of displacement of the tissue in response to a quasi-static periodic compression of the tissue.

[0040] It is thus a feature of at least one embodiment of the invention to provide image processing for standard elastography ultrasound acquisitions.

[0041] These particular objects and advantages may apply to only some embodiments falling within the claims, and thus do not define the scope of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

[0042] FIG. 1 is a simplified block diagram of an ultrasound imaging system for use with the present invention using a standard 2-D array ultrasound transducer as used with an optional RF ablation system providing an ablation probe for introduction into a tumor site of an in vivo organ and including a control system for applying a controlled reciprocity RF ablation probe for shear wave or quasi-static elastography imaging;

[0043] FIG. 2 is a simplified depiction of a geometry of a pattern of data acquisition that may be employed in the present invention showing an example with three angularly separated planes of data acquisition sharing a common axis;

[0044] FIG. 3 is a graph of the shear wave propagation along an x-axis as depicts noise in the data that can create artifacts during interpolation;

[0045] FIG. 4 is a graph similar to that of FIG. 3 showing tissue displacement at different points along the x-axis associated with quasi-static elastography and corresponding noise;

[0046] FIG. 5 is a top plan view of the data acquisition geometry of FIG. 2 showing bilinear cylindrical interpolation used in one embodiment of the invention over four angularly separated planes;

[0047] FIG. 6 is a simplified representation of an ultrasonic transducer for automatically acquiring data in the geometry shown in FIG. 2 by rotation of a 2-D ultrasound probe;

[0048] FIG. 7 is a figure similar to that of FIG. 6 showing a nonuniform 3-D ultrasonic probe for obtaining scattered data in the geometry of FIG. 2 such as is well accommodated by the present invention;

[0049] FIG. 8 is a simplified flowchart depicting the principal steps of the present invention in several embodiments;

[0050] FIG. 9 is a perspective diagram of two sub-blocks of the volume of interest attached together by a weighting process;

[0051] FIG. 10 is a diagram of adjacent data voxels showing the values used for the calculation of an approximation of gradient at a given voxel; and

[0052] FIG. 11 is a diagram showing adjacent spatial data points showing values used for the interpolation of voxel data to measured spatial data.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

General Description of the Hardware

[0053] Referring now to FIG. 1, an RF or microwave ablation probe 10 may be inserted percutaneously into a patient 12 along an axis 11 to have its tip located at an ablation region 16 within an organ 18, such as the liver. Extensible electrode tines 14, at the tip of the probe 10, may grip the tissue of the

ablation region and provide a greater area of electrical contact to conduct ablative current from a radiofrequency (RF) source **20**.

[0054] In this regard, electrical energy from the RF source **20** is conducted through an insulated shaft of the probe **10** to the conductive tines **14** where ionic heating of the tissue kills tumor tissue. A large-area grounding pad **31** placed on the patient's skin provides a return path for this current. The tines **14** may optionally include thermocouples for temperature measurements used to control the electrical energy to minimize the formation of a layer of high impedance charred tissue between the tines **14** and the tissue.

[0055] RF ablation probes **10** suitable for this purpose may include a single 17-gauge electrode, with a 2-3 cm long electrically active region at the tip embedded in tissue. These electrodes also offer the option of internally circulating chilled water during the ablation procedure to minimize the charring of tissue adjacent to the electrically active region of the electrode. RF ablation probes **10** of this kind having extensible tines and thermocouple sensors are known in the art and commercially available, for example, under the trade-name Valleylab Cool-Tip™ ablation electrode manufactured by Valleylab, CO, USA, or from other companies. The RF source **20** may be a Rita Model **30** electrosurgical device manufactured by Rita Medical Systems, Inc., Mountain View, Calif., or another similar device.

[0056] During the ablation process, electrical current is conducted from the RF source **20** along line **26** to the ablation probe **10**. The temperature signal is returned along line **24** to be received by the RF source **20** and used to limit the temperature of ablation according to techniques well understood in the art.

[0057] Imaging of the tissue and the tip of the probe **10** may be done using standard ultrasonic imaging system hardware, for example, the Siemens S2000 Real Time Scanner manufactured by Siemens, Inc. of California. The ultrasonic imaging system hardware may include an ultrasonic transducer **30** communicating with ultrasound processing circuitry **42**. The ultrasonic transducer **30** may be, for example, a one-dimensional ultrasonic transducer **30** (meaning that it has a one-dimensional array of individual transducer elements to acquire data over two dimensions) in the form of a linear array transducer approximately forty millimeters wide, operating with dynamic focus over a forty percent bandwidth and producing signals at a center frequency of five megahertz.

[0058] During insertion of the probe **10**, the ultrasound transducer **30** is placed against the skin of the patient **12** to emit a beam **36** of ultrasound directed into the patient **12** to acquire echo data along an imaging or data plane **34** extending from the ultrasound transducer **30** (seen edgewise in FIG. 1). After insertion of the probe **10**, the ultrasound transducer **30** may be used to monitor the ablation using elastographic imaging as will be described. During this monitoring and the subsequent elastographic imaging, the axis of the ultrasound transducer along which the ultrasound beam **36** propagates is aligned as closely as possible to the axis **11** along which the probe **10** extends. The probe **10** stabilizes the organ **18** and prevents lateral shifting along an axis perpendicular to axis **11**.

[0059] During both insertion of the probe **10** and the ablation process, an ultrasound beam **36** generated by the ultrasound transducer **30** travels into the tissue of the patient **12** and is reflected at various tissue structures and boundaries. These echoes are detected by the ultrasound transducer **30**

and conducted by cable **40** to the ultrasound processing circuitry **42**. The received signals are digitized at a sampling rate of approximately 50 megahertz and then processed according to techniques well known in the art to produce a sequence of two-dimensional images, for example, providing a constantly refreshed B-mode image on display terminal **44**.

[0060] A controller **46**, which may be a computer or logic controller programmed as described below, may also provide output lines **53** connected to a motorized carriage **52**, for example, using a motor and a lead screw (not shown) to provide motion of the probe **10** along its insertion axis **11** to reciprocate the probe **10** in a controlled manner according to signals on output line **53** as will also be described. Other mechanisms for implementing the motorized carriage **52**, including those which apply a predetermined compressive force or low-frequency oscillation, are also contemplated, for example, using an eccentric weight. In some embodiments, the controller **46** may also communicate with ultrasound processing circuitry **42** (or the display terminal **44** directly) for displaying images and receiving user input commands.

[0061] The digitized echo signals from the ultrasound transducer **30** are further processed either within the ultrasound processing circuitry **42**, or within controller **46**, to produce an elastographic image **41**. In the former case, line **48** communicates signals from the controller **46** to the ultrasound processing circuitry **42** to coordinate generation of the elastographic image; in the latter case, line **48** carries the control signals and digitized echo signals from the ultrasound processing circuitry **42** to the controller **46** for processing by the controller **46**.

Data Acquisition

[0062] Referring now to FIGS. 1 and 2, in a first embodiment, the ultrasound transducer **30** may be rotated about the probe **10** so as to rotate the data plane **34** about axis **11** while maintaining the plane **34** substantially aligned with axis **11**. This rotation allows the acquisition of echo data along multiple planes. In this example four planes **34a-d** are shown spaced from each other by 45 degrees. Other numbers of planes, for example, five and six equally or unequally spaced planes **34**, are also practical and there is generally no upper limit to the number of planes based on a trade-off between data acquisition and speed of reconstruction. Each of these planes **34** will provide multiple points of echo data over the surface of the plane **34**, each point of echo data described, for example, by a z-axis coordinate value (where the z-axis is aligned with axis **11**) and an x-axis coordinate value perpendicular to the z-axis and lying within the plane **34**. Together the planes **34a-d** are circumscribed within a cylindrical volume **60** that holds multiple C-planes **62** generally normal to axis **11** and spaced regularly along the z-axis. Generally, these planes may be acquired by beam steering or other techniques.

[0063] Referring momentarily to FIG. 8, in a first step of the invention, echo data of each plane **34** is processed to extract raw data necessary for elasticity measurements as indicated by process block **64**. The deduced elasticity may indicate absolute or relative elasticity of the tissue, and the raw data may be obtained using various different techniques. In a first technique, indicated by subprocess block **66**, the data of the planes **34** may be processed to acquire multicycle shear wave data as will now be described.

[0064] Referring to FIGS. 1 and 3, a reciprocating motion of the probe **10**, or other stimulation techniques such as ARFI, SSI and EVE and the like, may generate shear waves **68**

propagating perpendicularly to axis **11**, for example, radially away from that axis **11** as indicated by arrows **70**. Detection of the shear waves at each C-plane **62** may be performed by direct analysis of the radiofrequency ultrasonic signal or through the analysis of B-mode images to detect the displacement between successive images incident to the deformation of the shear wave **68**, for example, as described in U.S. Pat. No. 8,328,726 cited above. Generally the generation of B-mode imaging will not occur rapidly enough to track movement of the shear waves **68** along arrows **70** in real time but an effective reconstruction of that motion may be obtained by coordination between ultrasound processing circuitry **42** and the controller **46** reciprocating the probe **10** to obtain data of the data plane **34** capturing the shear waves **68** at multiple times, each time having a different phase delay with respect to the reciprocation of the probe **10**. Under the assumption that the shear waves **68** will be identical for each cycle of the reciprocation, this allows a piecewise reconstruction of the motion of the shear wave **68**. Alternatively, the entire image plane can be scanned using a plane acoustic wave to bypass the low imaging speed of B-mode acquisitions. Such plane acoustic wave acquisitions image the complete imaging plane in a single sweep, unlike the sequential focused technique used in B-mode acquisitions.

[0065] Propagation of the shear wave **68** in terms of arrival time at various locations along the x-axis may be plotted in a measurement curve **72** for each C-plane against different positions along the x-axis. The reciprocal of the slope of the measurement curve **72** will generally indicate the velocity of the shear wave **68** providing information about elasticity of the propagating medium. The substantial noise component in the measurement curve **72** presents a problem with respect to differentiating this measurement curve **72** in order to obtain velocity. Samples **73** of this measurement curve **72** will be acquired per process block **64** of FIG. **8** to be discussed below.

[0066] Referring now to FIGS. **4** and **8**, in an alternative technique, the acquired ultrasound data at process block **64** may indicate a z-axis displacement of the tissue with reciprocation of the probe along axis **11** or other stimulation of the tissue along axis **11**; for example, ultrasonic stimulation may be used to deduce tissue movement within a cycle of stimulation according to standard dynamic or quasi-static elastography. Again, a measurement curve **80** providing a measure along the x-axis for each C-plane **62** may be obtained and sampled to provide for the acquired elasticity data at process block **64** of FIG. **8**.

Determining Voxel Data

[0067] Referring now to FIGS. **5** and **8**, the samples **73** may lie along intersection lines **84** between the planes **34** and each C-plane **62** to provide for multiple points of elasticity spatial data **86** spaced along each of the lines **84** within each C-plane **62**. This acquired data of the samples **73** will be termed “spatial data” and designated by values “b” to distinguish it from data of voxels which will be determined from the spatial data and designated by values “c”.

[0068] Generally, the present invention determines values of the voxels **88** so that when the values of the voxels **88** are interpolated to the locations of actual spatial data **86**, the two values match (interpolation fidelity). The interpolation may use, for example, a trilinear interpolation among the voxels **88** surrounding given spatial data **86**.

[0069] As will be seen, this interpolation fidelity is balanced against a requirement for smoothness in the data of the

voxels **88**, meaning generally that the data of the voxels **88** changes slowly over space in the manner to be expected when measuring the elastic properties of physical tissue which will tend to be homogenous within any given region.

[0070] Referring now to FIG. **11**, an element of spatial data **86** may be compared to a trilinear interpolation of the data of voxels **88** as shown as the vertices of a simple polyhedron (e.g., a cube) surrounding the element of spatial data **86**. As is understood in the art, trilinear interpolation will first perform linear interpolation, for example, between voxels **88** at points cool and coo, being two vertices of the polyhedron, to obtain a value c_{01} along one edge of the polyhedron between the two vertices at a location along the edge generally aligned with one coordinate of the spatial data **86**—in this case the x-coordinate. Similar interpolation is conducted for each edge of the polyhedron parallel to the above edge to obtain first interpolation values c_{11} , c_{00} , c_{10} . Linear interpolation is then performed between corresponding pairs of these interpolated values to provide second interpolation values (c_1 , c_0) aligned with a second coordinate of the spatial data **86**—in this case the y-coordinate. Finally the third interpolation will be performed between the second interpolated values to provide a third interpolation value c for the spatial data **86**. The difference between this third interpolation value c and the actual spatial data **86** will desirably be minimized.

[0071] Generally this interpolation process can be represented as follows:

$$c = k_{000}c_{000} + k_{001}c_{001} + \dots + k_{111}c_{111} \quad (1)$$

where the coefficients k are interpolation weights that may be collected into a matrix A having eight non-zero entries in each row corresponding to the eight interpolation weights; the number of rows equal to the number spatial data points; and the number of columns equal to the number of voxels.

[0072] Referring now to FIG. **10**, the present invention also seeks to enforce smoothness on the selected values of voxels **88**. In one embodiment, the smoothness may be enforced by constraining the second derivative (Laplacian) at each of the voxel values. The second derivative can be approximated by the second order central differences as follows:

$$\frac{d^2 c}{dx^2}(x, y, z) \approx c_{011} - c_{00-1} + 2c_{000} \quad (2)$$

$$\frac{d^2 c}{dy^2}(x, y, z) \approx c_{010} - c_{0-10} + 2c_{000} \quad (3)$$

$$\frac{d^2 c}{dz^2}(x, y, z) \approx c_{100} - c_{-100} + 2c_{000} \quad (4)$$

[0073] The Laplacian is then given by:

$$\nabla^2 c = \frac{d^2 c}{dx^2} + \frac{d^2 c}{dy^2} + \frac{d^2 c}{dz^2} \quad (5)$$

where the coefficients of equations (2)–(4) of +1, -1, and 2 may be entered into a matrix B so that the matrix vector product Bc provides the vector of the Laplacian derivative over the entire grid. Matrix B will generally be a square matrix with seven non-zero entries per rows and the number of columns equal to the number of voxels.

[0074] The present invention may then compute the values c for each voxel by choice of c to minimize:

$$\|Ac-b\|^2 \quad (6)$$

subject to

$$\|Bc\|^2 \leq M \quad (7)$$

[0075] where:

[0076] c is the voxel data to be determined;

[0077] b is the known spatial data proximate to the voxels;

[0078] A is an interpolant matrix performing a linear interpolation of values c to the location of data points in b ;

[0079] B is a finite differencing gradient matrix providing the gradient in data of the voxels; and

[0080] M is a constant selected to describe the desired image smoothness.

[0081] Here the symbol $\|\cdot\|$ denotes the 2-norm of the vector (i.e., the square root of the sum of the square of the entries).

[0082] An unconstrained version of this minimization problem may be represented as follows:

$$\text{minimize } \|Ac-b\|^2 + \lambda \|Bc\|^2 \quad (8)$$

where λ provide a weighting rather than a hard limit. This problem of equation (8) has a closed form solution given by:

$$c = (A^T A + \lambda B^T B)^{-1} A^T b \quad (9)$$

[0083] where T denotes a matrix transposition.

[0084] This matrix inverse is not explicitly calculated, but instead a sparse linear solver routine may be used which solves the system of equations:

$$(A^T A + \lambda B^T B) c = A^T b \quad (10)$$

for the unknowns in c . The system of equations can be solved rapidly even for large grid sizes with over 1 million grid points because the matrices are sparse with only a few nonzero entries near the diagonal (also called a banded diagonal structure). The banded diagonal structure is a consequence of the vectorization of the 3-D points into a one-dimensional vector c .

[0085] While the value of λ maybe predetermined it will be understood that it may also be selected by cross-validation of the data, without the user having to specify the value of λ in advance.

[0086] Referring now to FIG. 8, this solution process is indicated generally by process block 67.

[0087] Referring now to FIG. 9, the ability to rapidly solve equation (10) can be enhanced by allowing all of the necessary matrix and vector values to be stored in low latency memory (e.g., RAM). This can be ensured by dividing a region of interest 101 encompassing all of the relevant spatial data b into one or more sub-blocks 105a, 105b, etc. and by separately processing each sub-block 105 with equation (10). The sub-blocks may then be "stitched" together by blending peripheral voxel data 90 (representing overlapping spatial locations) using, for example, weighting values 107 of w_0 and w_1 on respective sub-blocks 105, each weight slowly decreasing the weighting of the data of one sub-block 105 as one moves toward the adjacent sub-block 105. In this regard, the two weighting values 107 may be selected so that they always sum to unity.

[0088] Referring now to FIG. 6, in one embodiment, movement of the ultrasonic transducer 30 may be automated by mounting a one-dimensional or 1.5 D ultrasonic transducer 30 on an axially reciprocating carriage 100, for example,

driven by electric actuator 103 under the control of controller 46 (shown in FIG. 1). The transducer 30 may provide, for example, one (for a one-D probe) or a small number, such as three, rows of ultrasonic elements 106 (for a 1.5-D probe) each of which may be separately actuated for phased array or other imaging modes to transmit portions of the ultrasound beam 36 and to be independently readable to receive echo signals in return. The multiple rows of ultrasonic elements help provide for focusing of the ultrasound into a substantially planar ultrasound beam 36. The reciprocating carriage 100 may rotate the ultrasonic transducer 30 about axis 11 substantially mimicking the motion described above with respect to FIG. 1 while providing improved orientation of the resulting ultrasound beam 36 along the axis 11. The reciprocating action, for example, may move the ultrasonic transducer 30 by 180 degrees in one direction and then backward to its initial starting position to obtain the sheaf of data planes 34 described with respect to FIG. 2. A center of the ultrasonic transducer 30 may provide for an opening 102 through which the probe 10 may pass to permit for this improved orientation of the ultrasound beams 36 with the axis 11 while sacrificing only one center ultrasonic element 106 of the ultrasonic transducer 30 in an area which is generally oversampled. A simplified motorized carriage 52 is shown providing for vertical reciprocation along axis 11 of the probe 10 also under control of controller 46.

[0089] Referring now to FIG. 7, in an alternative embodiment, a modified two-dimensional array 104 may be created having scattered ultrasonic elements 106 positioned as needed for the acquisition of the multiple planes 34 without movement of the two-dimensional array 104. For example, the ultrasonic elements 106 may be placed along diagonal lines arrayed radially from axis 11 with a 45-degree spacing. This sparse ultrasound array reduces the number of channels necessary for data acquisition while still providing the rapid 3-D reconstruction of the present invention.

[0090] It will be appreciated that the spacing of the ultrasonic elements 106 along the lines perpendicular to the axis 11 of the ultrasonic elements 106 may be varied, for example, to reduce the element density toward the center of the array in favor of those ultrasonic elements 106 further outward for improved imaging resolution away from the center. The array 104 may be combined with the reciprocating carriage 100 to create a hybrid system.

[0091] It will be appreciated that the present invention may be combined with techniques to measure temperature of an ablated region, for example, as described in U.S. Pat. No. 7,166,075 hereby incorporated by reference. In this regard, the spatial data 86 may be generally scattered as in a cloud without regard to regular grid locations used for image display. The present invention is particularly suited for scattered and/or sparse data of this type allowing the location of the spatial data 86 to be freely acquired or readily tailored to regions of interest.

[0092] It will be appreciated that the present invention may be used advantageously with parametric imaging techniques on radiofrequency, or B-mode data, for 3-D quantitative ultrasound imaging. In addition, the invention can be used with color/power Doppler systems, for example, to produce a three-dimensional representation of blood flow. The invention is not limited to the probes described above and can be used, for example, with a planar, two-dimensional ultrasound array.

[0093] It will be further appreciated that the present invention may be used advantageously with standard imaging techniques such as B-mode, color and power Doppler imaging and the like for ablation techniques in which the simplification of the imaging acquisition provides for good reconstruction of ablation masses and for other high-speed 3-D visualization such as blood flow for 3-D vascular imaging. It will be appreciated that the invention is not limited to linear interpolation but also higher order (e.g. tricubic) interpolations may be used. Similarly the smoothness requirements can be enforced using the first derivative (first order finite differences) or higher order central differences.

[0094] It is specifically intended that the present invention not be limited to the embodiments and illustrations contained herein, but include modified forms of those embodiments including portions of the embodiments and combinations of elements of different embodiments as come within the scope of the following claims.

We claim:

1. An apparatus for acquiring three-dimensional ultrasound data comprising:

an ultrasonic probe assembly adapted to direct an ultrasound beam into tissue and receive ultrasonic echoes and measure the same to provide ultrasound data; and

an electronic computer receiving the ultrasound data and executing a stored program held in non-transitive medium to:

(a) process the ultrasound data to obtain spatial data characterizing the tissue at a plurality of discrete locations over three dimensions of a volume of interest within the tissue; and

(b) determine data of voxels in a three-dimensional image grid within the tissue by simultaneously minimizing a combination of:

an error between data of voxels interpolated to the locations of the spatial data for voxels in a region proximate to the spatial data; and

a gradient of the data of the voxels at the location of each voxel;

wherein the region proximate to the spatial data extends in three dimensions about the spatial data by less than the dimensions of the volume of interest.

2. The apparatus of claim 1 wherein the error in interpolation is a function of a magnitude of a difference between a value of a given element of spatial data and an interpolated value of surrounding voxels to the location of the spatial data in three dimensions.

3. The apparatus of claim 1 wherein the gradient is a function of differences among data of voxels adjacent to the given voxel.

4. The apparatus of claim 1 wherein the determination is performed by selecting a value of given voxel data to minimize:

$$\|Ac-b\|^2$$

subject to

$$\|Bc\|^2 \leq M$$

where: c is a vector of the data of the given voxels to be determined;

b is a vector of the known spatial data;

A is an interpolant matrix performing a linear interpolation of values c to the locations of data points in b;

B is a finite differencing gradient matrix providing the gradient in data of the voxels; and

M is a constant selected to describe the desired image smoothness.

5. The apparatus of claim 4 wherein A is a sparse matrix.

6. The apparatus of claim 1 wherein the determination solves a closed form expression:

$$c=(A^TA+\lambda B^TB)^{-1}A^Tb$$

where:

c is the voxel data to be determined;

b is the known spatial data surrounding the voxels;

A is an interpolant matrix performing a linear interpolation of values c to the locations of data points in b;

B is a finite differencing gradient matrix providing the gradient in data of the voxels; and

λ is a predetermined value controlling the amount of smoothing of the data.

7. The apparatus of claim 1 wherein a number of points of spatial data within the volume of interest is less than a number of voxels within the volume of interest.

8. The apparatus of claim 1 wherein the region proximate to the spatial data extends to no more than a closest eight voxels.

9. The apparatus of claim 1 wherein the voxels are located at regular intervals along three Cartesian dimensions and the region proximate to the spatial data is a smallest polyhedron that surrounds the spatial data with voxels at vertex points and wherein the error is calculated only from interpolation from these vertex spatial data points.

10. The apparatus of claim 9 wherein the interpolated values are trilinear interpolation in three dimensions.

11. The apparatus of claim 1 wherein the volume of interest is subdivided into sub-blocks and step (b) is repeated for multiple sub-blocks and those blocks combined by weighting data at a periphery of adjacent sub-blocks.

12. The apparatus of claim 1 wherein the spatial data characterizing the tissue is a speed of a shear wave through the tissue at the points of spatial data.

13. The apparatus of claim 1 wherein the spatial data characterizing the tissue is a function of displacement of the tissue in response to a quasi-static periodic compression of the tissue.

14. A method of acquiring three-dimensional ultrasound data using an ultrasonic probe assembly adapted to direct an ultrasound beam into tissue and receive ultrasonic echoes and measure the same to provide ultrasound data comprising the following steps executed on an electronic computer receiving the ultrasound data and executing a stored program held in non-transitive medium to:

(a) process the ultrasound data to obtain spatial data characterizing the tissue at a plurality of discrete locations over three dimensions of a volume of interest within the tissue; and

(b) determine data of voxels in a three-dimensional image grid within the tissue by simultaneously minimizing a combination of:

an error between data of voxels interpolated interpolating to the locations of the spatial data for voxels in a region proximate to the spatial data; and

a gradient of the data of the voxels at the location of the given voxel;

wherein the region proximate to the spatial data extends in three dimensions about the spatial data by less than the dimensions of the volume of interest.

15. The method of claim **14** wherein the determination is performed by selecting a value of data of a given voxel to minimize:

$$\|Ac-b\|^2$$

subject to

$$\|Bc\|^2 \leq M$$

where:

c is the voxel data to be determined;

b is the known spatial data proximate to the voxels;

A is an interpolant matrix performing a linear interpolation of values c to the locations of data points in b; and

B is a finite differencing gradient matrix providing the gradient in data of the voxels; and

M is a constant selected to describe the desired image smoothness.

16. The method of claim **15** wherein A and B are both sparse matrices.

17. The method of claim **15** wherein the determination solves the closed form expression:

$$c=(A^TA+\lambda B^TB)^{-1}A^Tb$$

where:

c is the voxel data to be determined;

b is the known spatial data proximate to the voxels;

A is an interpolant matrix performing a linear interpolation of values b to the location of c;

B is a finite differencing gradient matrix providing the gradient in data of the voxels; and

λ is a predetermined value controlling the amount of smoothing of the data.

18. The method of claim **14** wherein a number of points of spatial data within the volume of interest is less than a number of voxels within the volume of interest.

19. The method of claim **14** wherein the region proximate to the spatial data extends only to a closest eight voxels.

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